

FAST ORBIT CORRECTION AT THE ESRF

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Orbit stability requirement

1 ESRF is a 3rd generation light source:

Energy: 6GeV

Circumference: 844.39m / 32cells

Horizontal and vertical emittance: 4nm and 30pm

1 *Position stability must match this emittance figure*

1 Stability criterion

Less than 20% emittance growth or:

<10% beam size increase

<10 % beam divergence increase

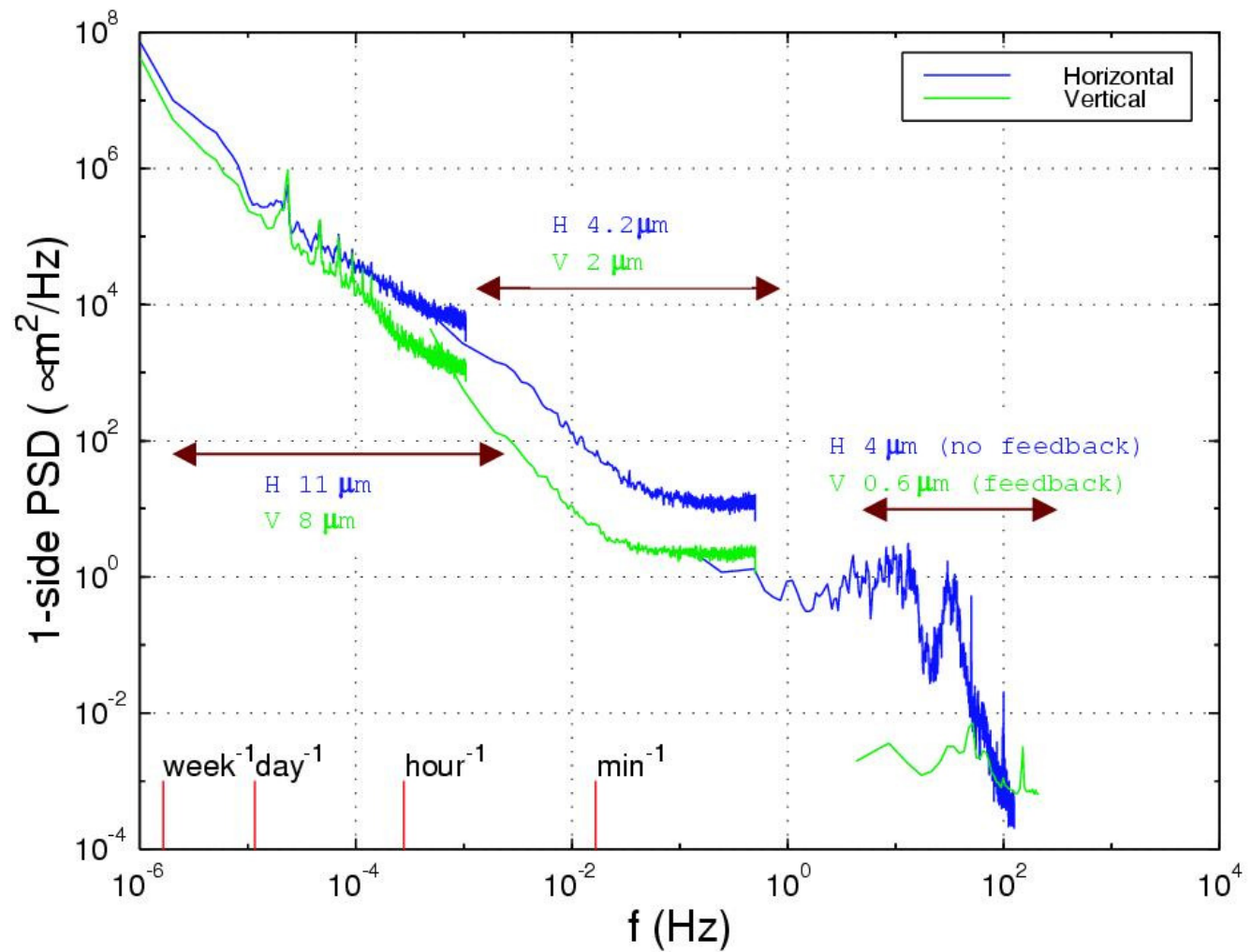
More stringent demands at high frequency from some beamlines

Beam stability at ESRF (until Nov. 2004)

Beam motion on straight sections BPMs

: $\beta_x=35.4\text{m}$, $\beta_z=6.2\text{m}$

$\sigma_x=360\mu\text{m}$, $\sigma_z=15\mu\text{m}$



FAST/SLOW correction management:

- 1 **ESRF solution:**
 - 1 *2 independent systems:*
 - 1 **Slow system with 224 BPMs/96 correctors from 0 to .1Hz**
 - 1 **Fast systems from .2 to 100 Hz**
 - 1 **Frequency separation between the slow and fast system**
 - 1 **Addition of a feed forward angle corrections during ID gap change on some straight sections to improve the orbit settling time in the .2 to .02 Hz range**
 - 1 **Choice due to circumstance, but it works fine**

We have recently upgraded our fast global feedback to damp the horizontal and vertical orbit distortions from .1 to 200Hz

Situation before the global feedback upgrade

1 Vertical global feedback system

- Aimed at bringing back the fast vertical motion to less than 10% of the beam size
- 20 nm/Hz^{1/2} BPM resolution (1 μm in 2 KHz BW)
- .1 to 150 Hz feedback bandwidth
- (separation from the slow correction in the frequency domain)
- 4.4 KHz sampling and correction rate
- Air cored magnets and 2mm thick stainless steel vessel
- low signal latency in the loop: .6mS

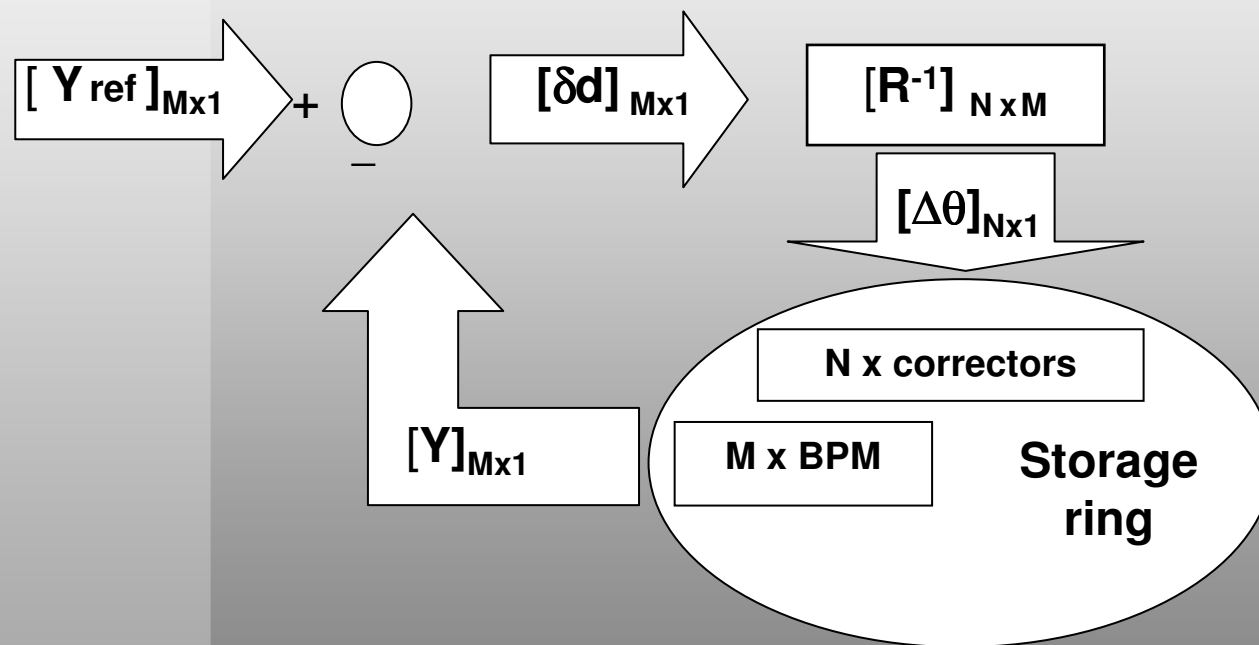
1 4 horizontal local feedback systems

Installed from 1999 to 2001 on sensitive beam lines:

- 1 ID14: Protein cristallography
- 1 ID21: X-ray microscopy
- 1 ID8: soft X ray spectroscopy
- 1 ID24 X ray absorption spectroscopy

Same type of BPMs and steerers as the global feedback

Global closed orbit correction principle

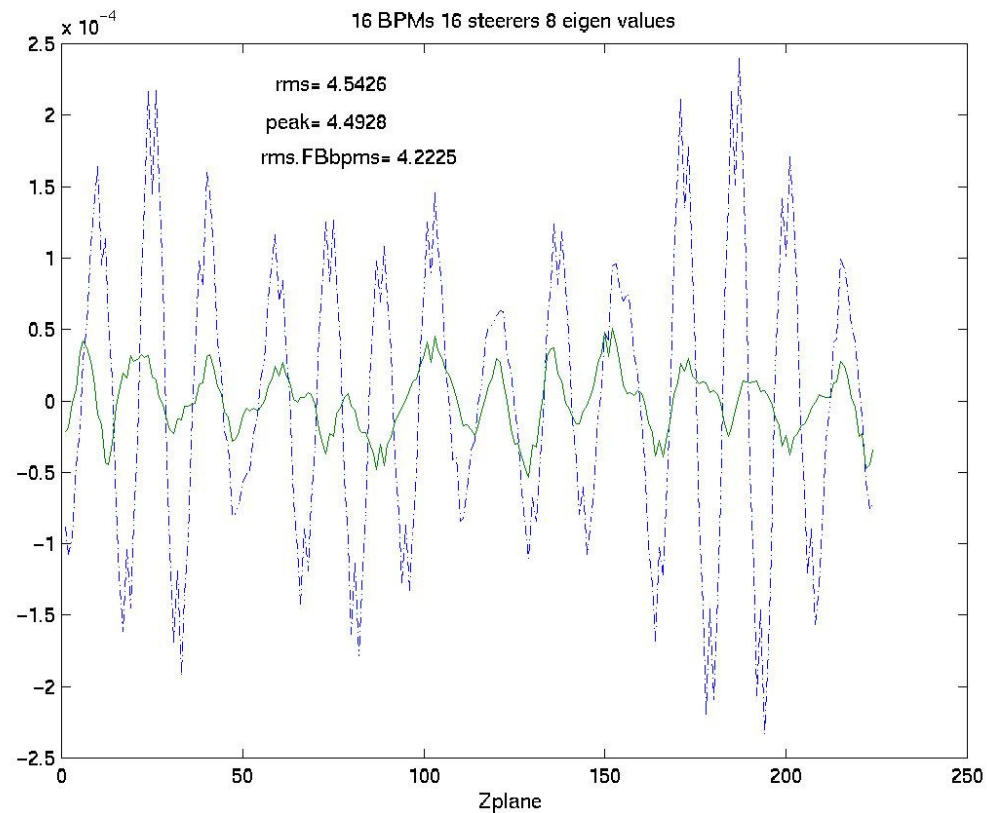


$$\text{Corrected orbit} = ([Y]_{M \times 1} - [Y_{ref}]_{M \times 1}) - R_{M \times N} \times [\Delta \theta]_{N \times 1}$$

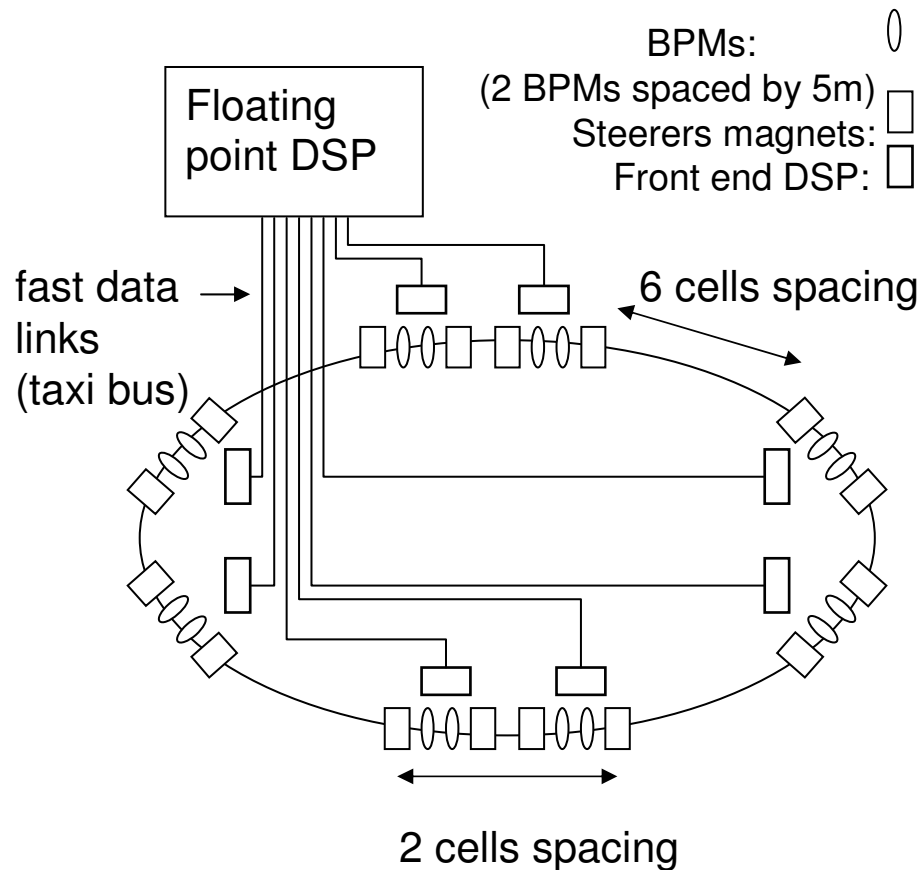
$[R^{-1}]_{N \times M}$ is obtained by a SVD method

efficiency

- 1 a limited number of monitors and correctors can correct all the machine => global scheme = undersampling
- 1 According to simulations 16 monitors and correctors are enough in the vertical plane ($Q=14.39$)
- 1 Rule of thumb: Number of BPM corrector needed = Q



Vertical global feedback layout



Vertical correction only

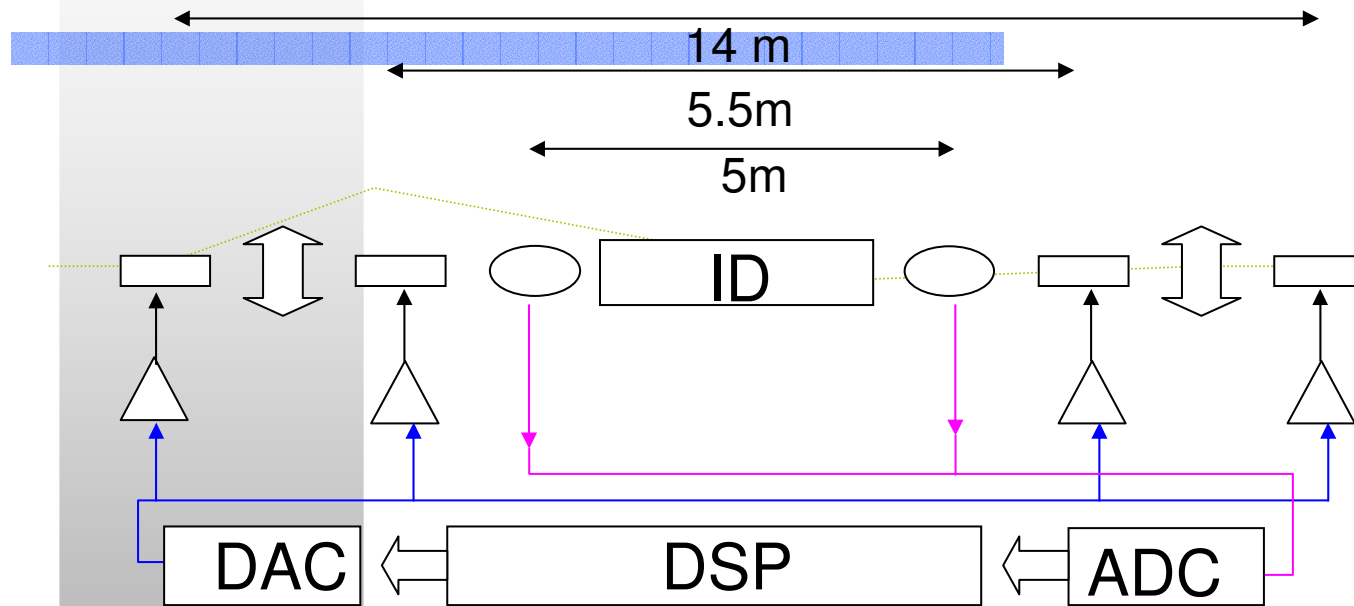
4.4 KHz sampling and correction rate





150 Hz feedback bandwidth

**Achieved damping: 2
(.1 to 100 Hz)**

**Residual movement:
12% of the beam size**

Local feedback layout



-  BPM electrodes
-  Quadrupole triplet
-  Corrector magnet
-  Amplifier

20 nm/Hz^{1/2} BPM resolution (1 μm in 2 KHz BW)

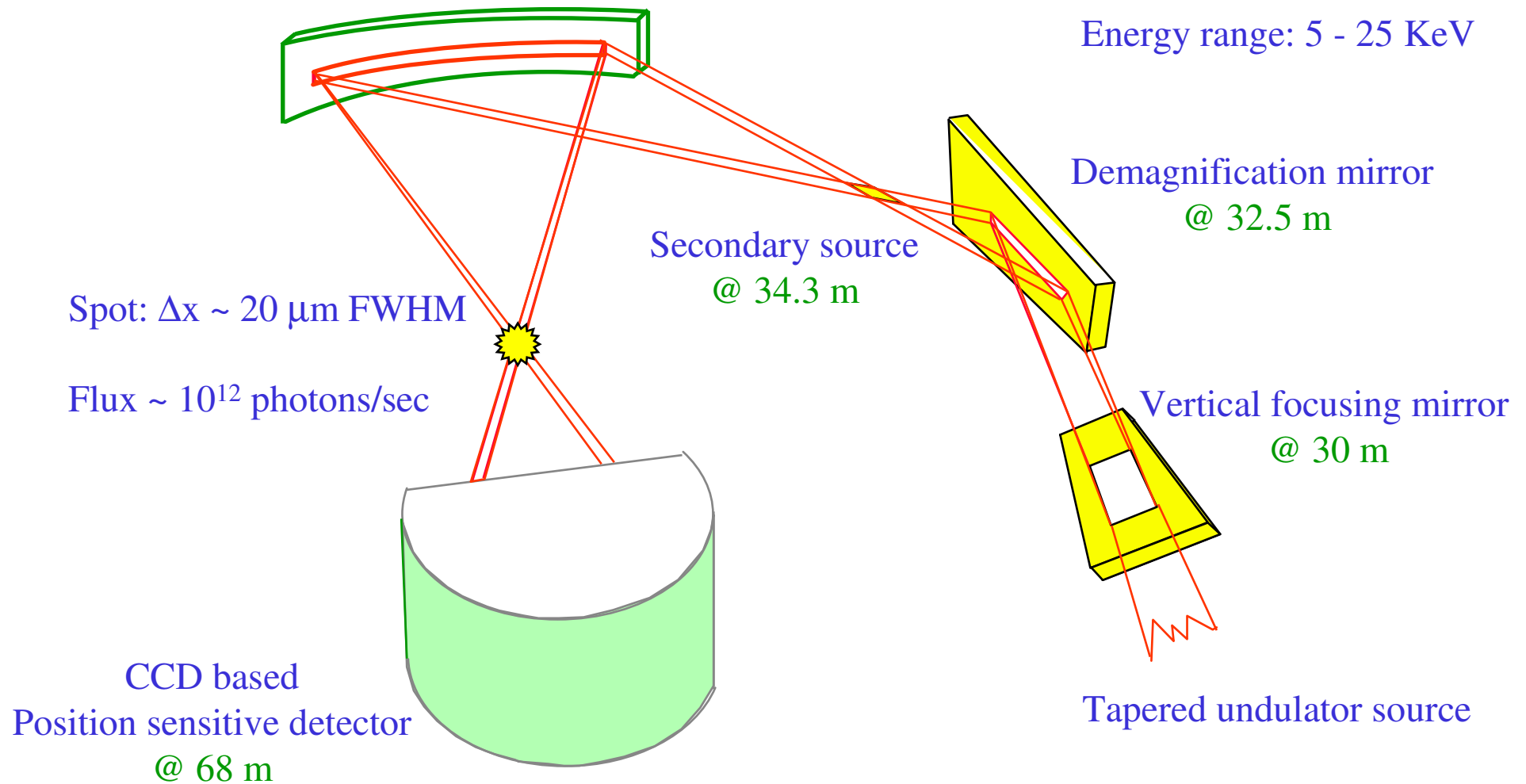
4.4 KHz sampling and correction rate

.1 to 150 Hz feedback bandwidth

Factor 4 damping (with our beam spectrum)

Separation from the slow correction in the frequency domain

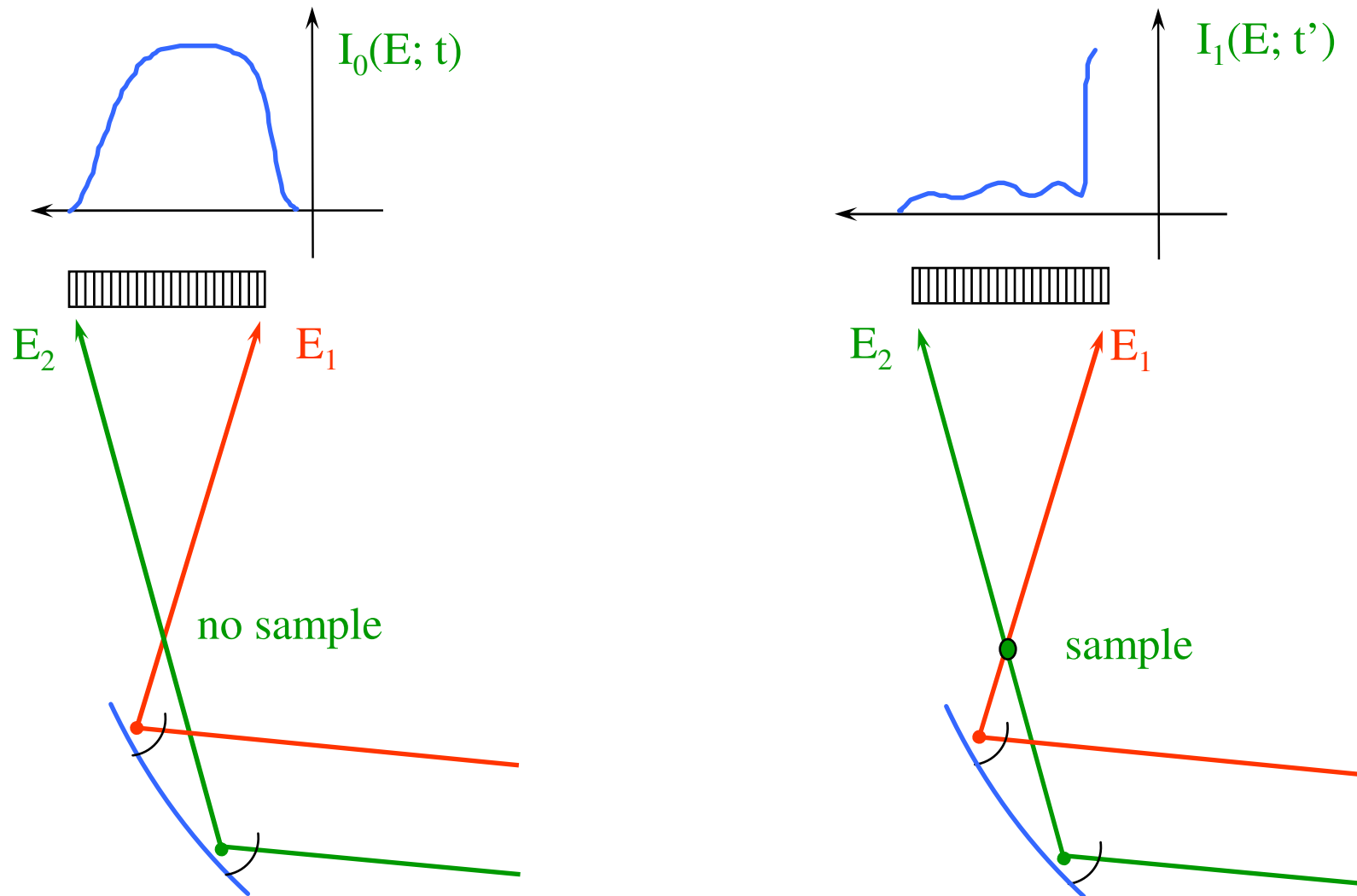
Si(111) or Si(311) Bragg/Laue polychromator @ 64 m



Beamline ID24

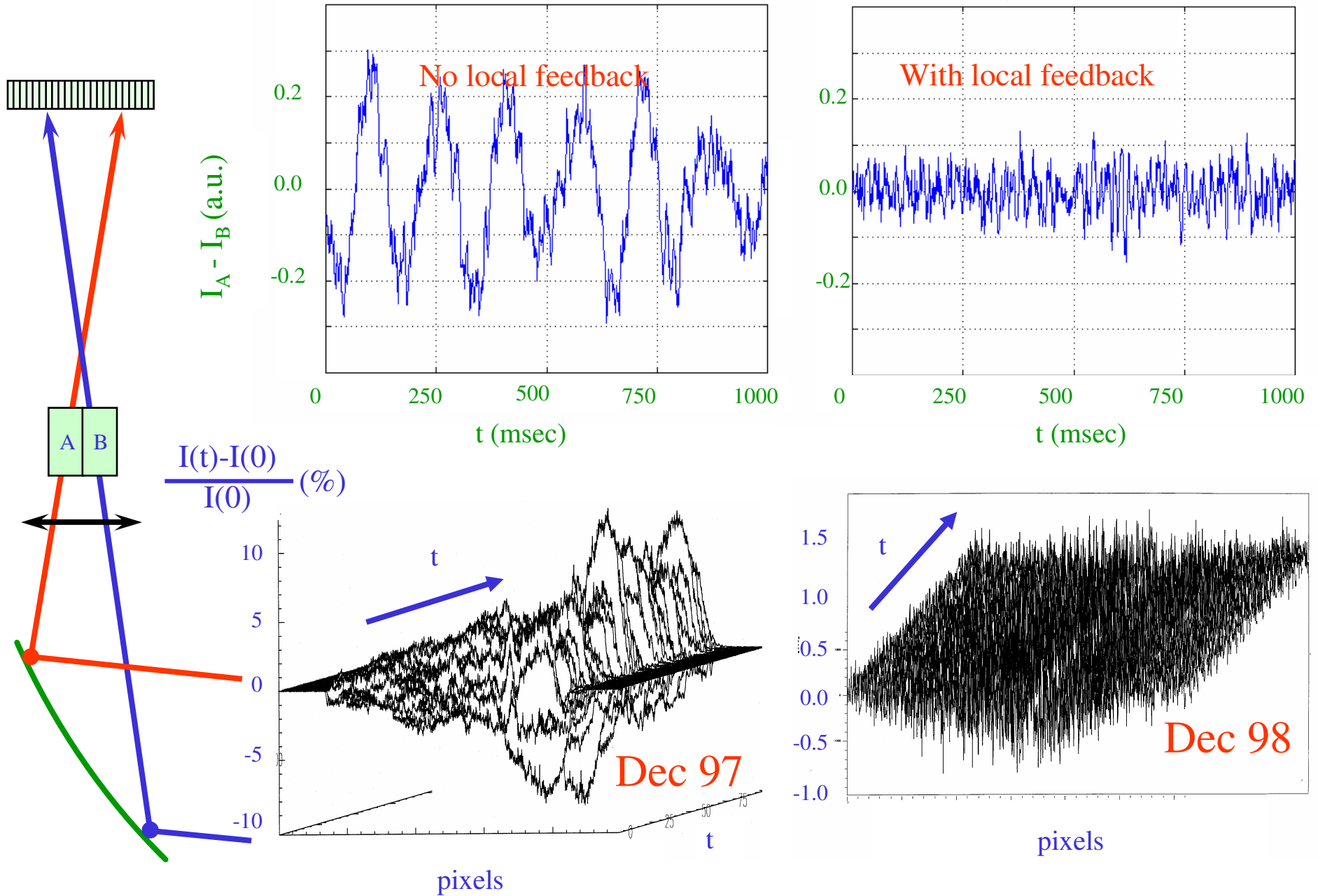
- 1 X ray Absorption Spectroscopy
- 1 All the absorption spectrum is recorded simultaneously thanks to a polychromator

The measurement of the absorption coefficient $\mu(E)$

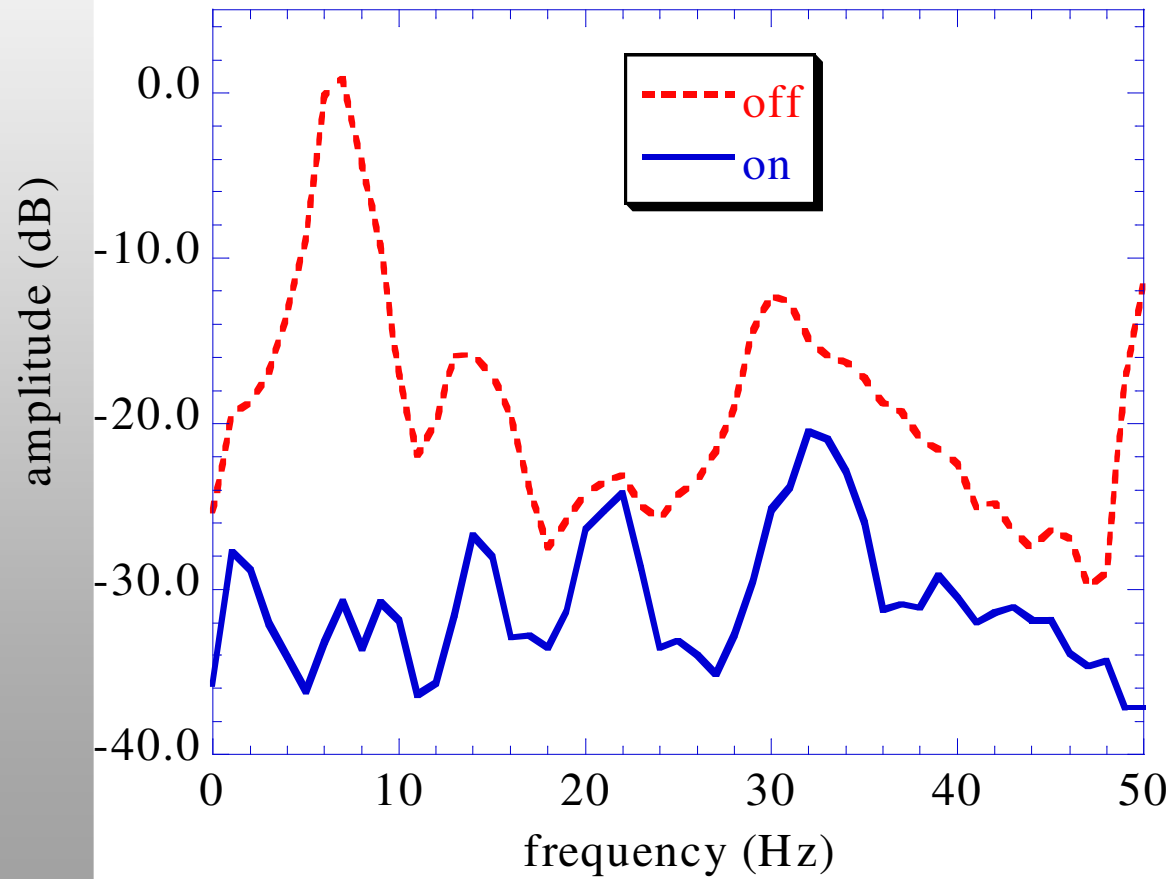


$$I_1(E) = I_0(E) e^{-\mu(E)d} \quad \Rightarrow \quad \mu(E) d = \ln \frac{I_0(E)}{I_1(E)}$$

EFFECT OF THE LOCAL FEEDBACK

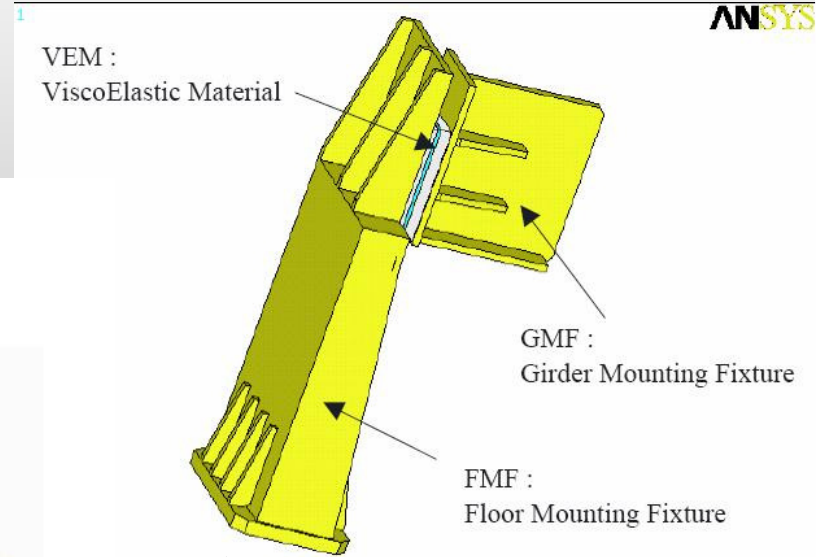


Spectrum of the motion on the sample:

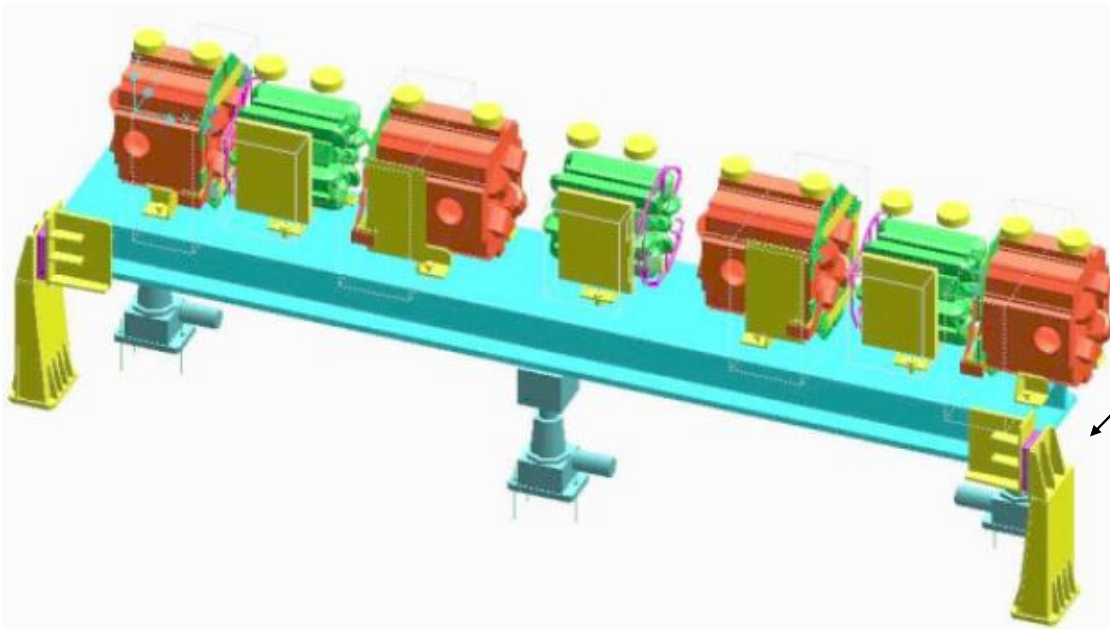


Damping pads on the magnets girders

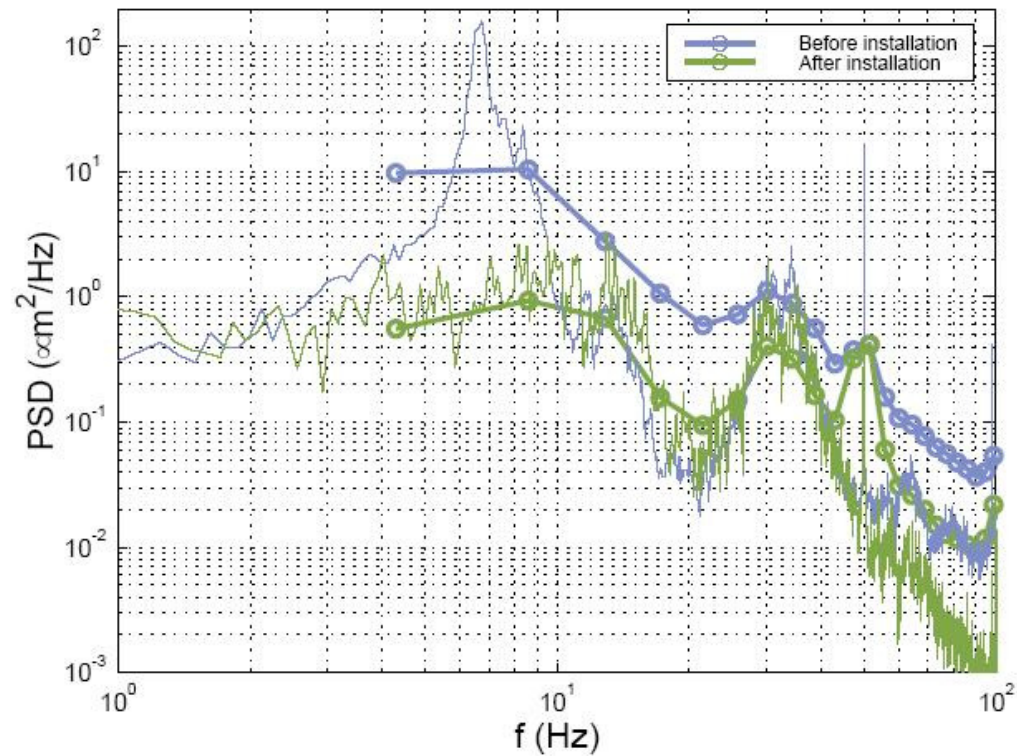
ANSYS



Damping link design



Damping pads on the magnets girders



Effect of damping links on the horizontal beam motion

- -20dB reduction of the 7Hz
- less reduction of the 30Hz:
it is due to the water flow in
the quadrupoles coils

Feedforward correction: ID gap dependant CO distortion

- 1 **A good solution for the .03 to 3Hz span without feedback**
- 1 **Used to take care of the transient orbit distortion due to the gap change of some insertion devices:**
 - 1 **Measurement of the closed orbit distortion for every ID gap opening values during calibration sessions**
 - 1 **Calculation of a correction using 2 correction dipoles at both end of the straight section for every gap opening values**
 - 1 **Application of this additional correction as a function of the gap opening in operation (update rate of the correction: 10Hz)**

Limitation of our correction system

1 Vertical global feedback system

Victim of the success of the damping pads installation:
The resolution of the BPMs was now too close to the amplitude of the vertical beam motion without feedback!

1 horizontal local feedback systems

ID24 X ray Absorption Spectroscopy beamline got the first system

Others beam lines requested horizontal correction:

Eventually crosstalk between the systems due to imperfect bump closure at high frequency started to appear, setting a limit to the number of local feedback systems, but not to the number of beam lines interested by a feedback....

Global feedback upgrade

2001 situation:

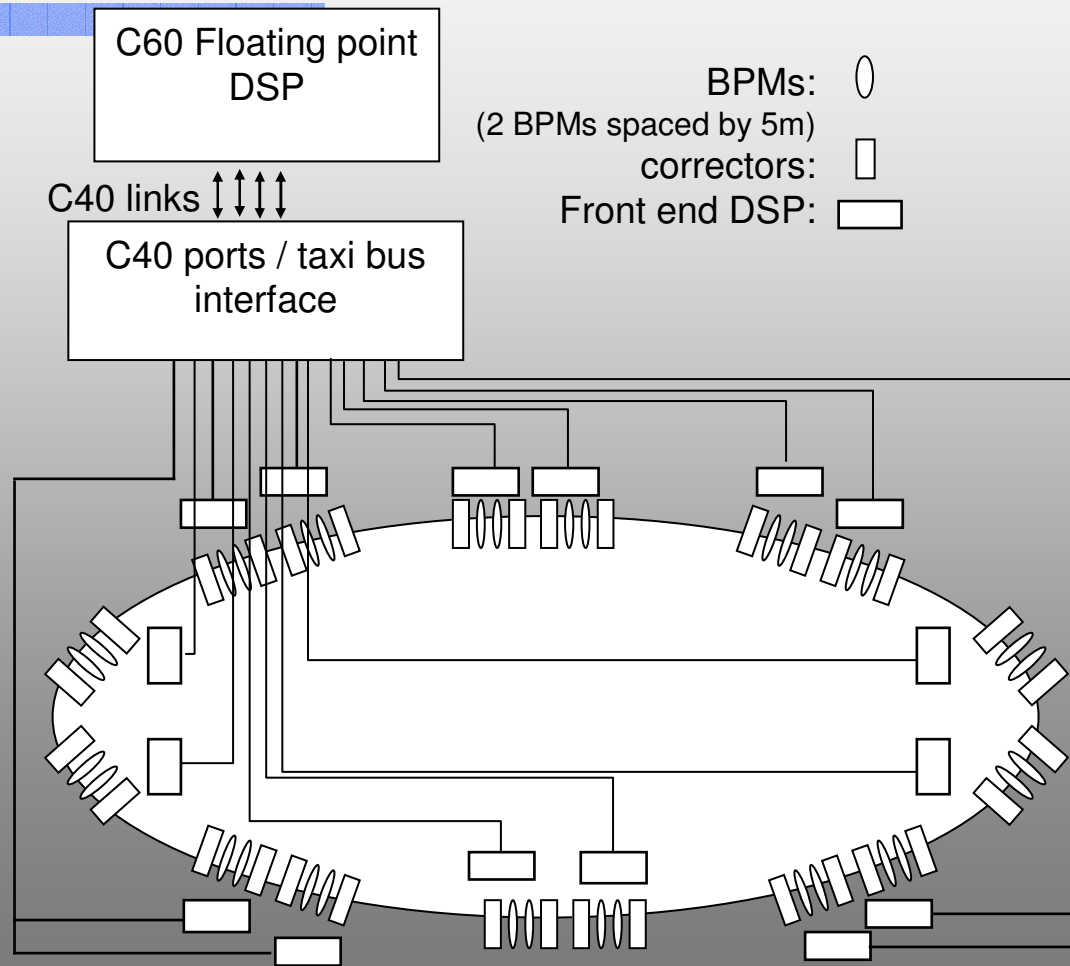
- 1 We want to improve the resolution of the vertical orbit distortion measurement
- 1 We wish to have the same low horizontal beam motion amplitude as in the straight sections corrected by the local feedback all over the machine

Solution:

- 1 We need a global feedback in both planes (no more local feedbacks).
- => We must increase the number of BPMs and correctors (since $Q_x=36.44$) and the DSP processing power

upgraded Global feedback

32BPMs
24 correctors
vertical and horizontal correction



Upgraded system features

- 1 Same components as in the first system:
- 1 RF multiplexing BPMs
- 1 Taxi bus data links
- 1 New DSP: TI C67 in replacement of the TI C40

Commissioning during 2004, now in operation

Feedback efficiency

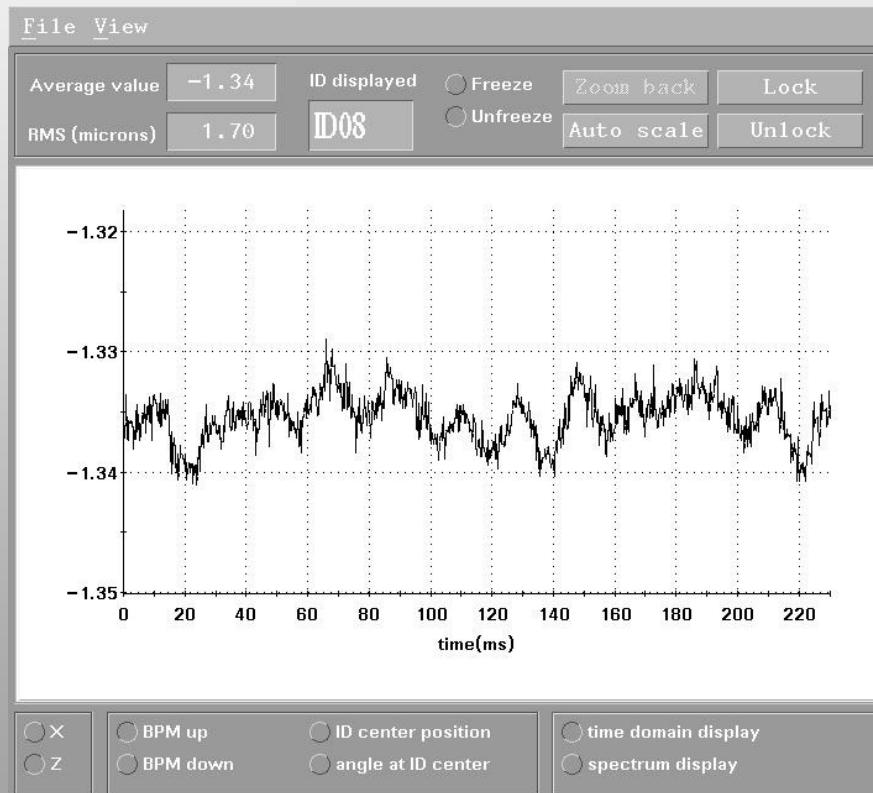
measured at the end of high horizontal β straight section

	β (in m)	rms motion without feedback (in μm , .1 to 200Hz)	rms motion with feedback (in μm , .1 to 200Hz)	rms motion/ rms size
H plane	36	5 to 12 (depending on BPM)	1.5 to 2.5 (depending on BPM)	.004 to .006
V plane	6.5	1.5 to 2.5 (depending on BPM)	.8 to 1.2 (depending on BPM)	.1

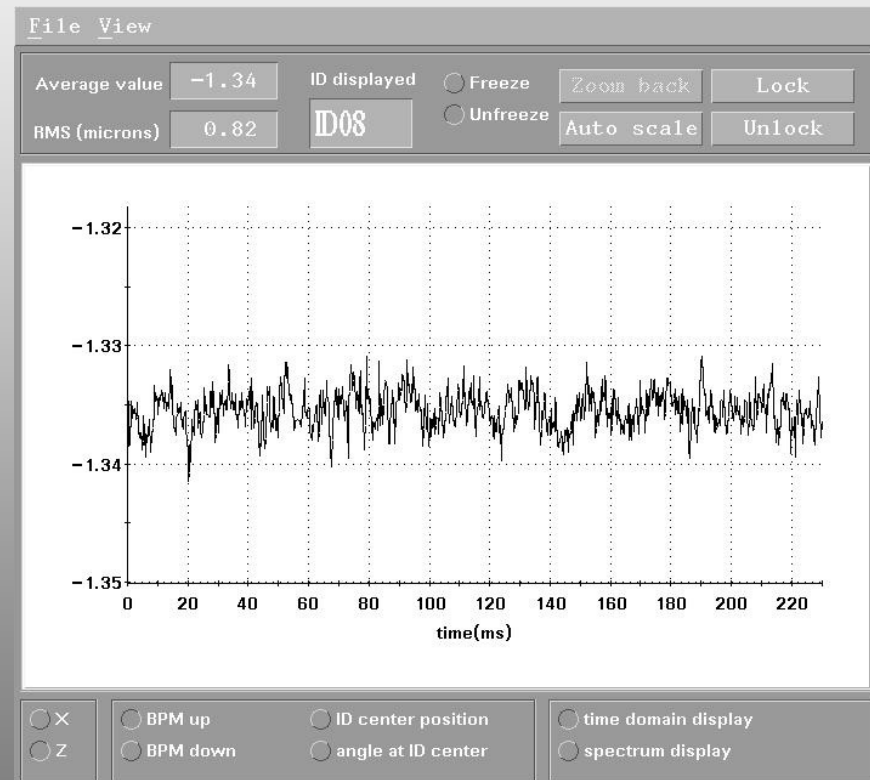
Feedback bandwidth: .1Hz to 150 Hz

Beam H and V emittance: 4nm and .03nm

V plane results:



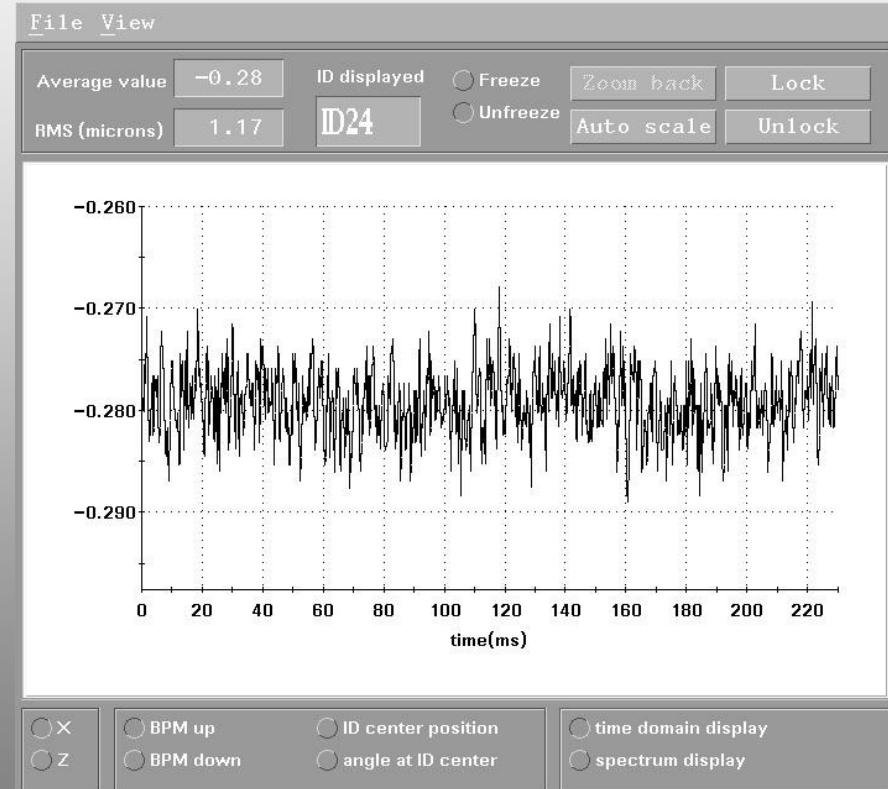
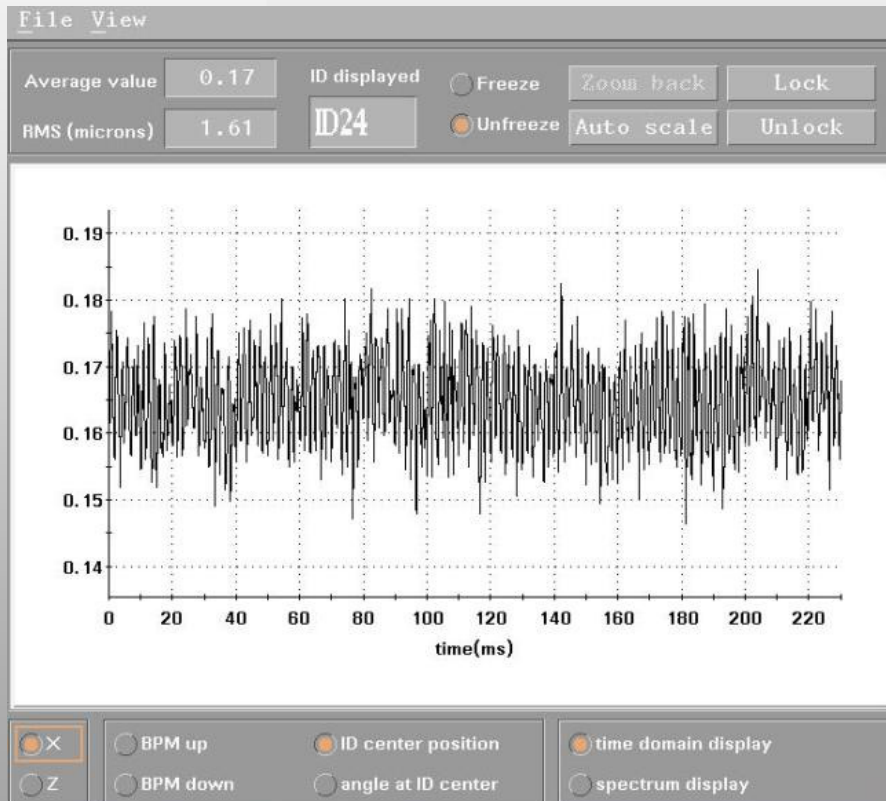
Left: feedback OFF



Right: feedback ON

rms value: integrated from .1 to 200Hz

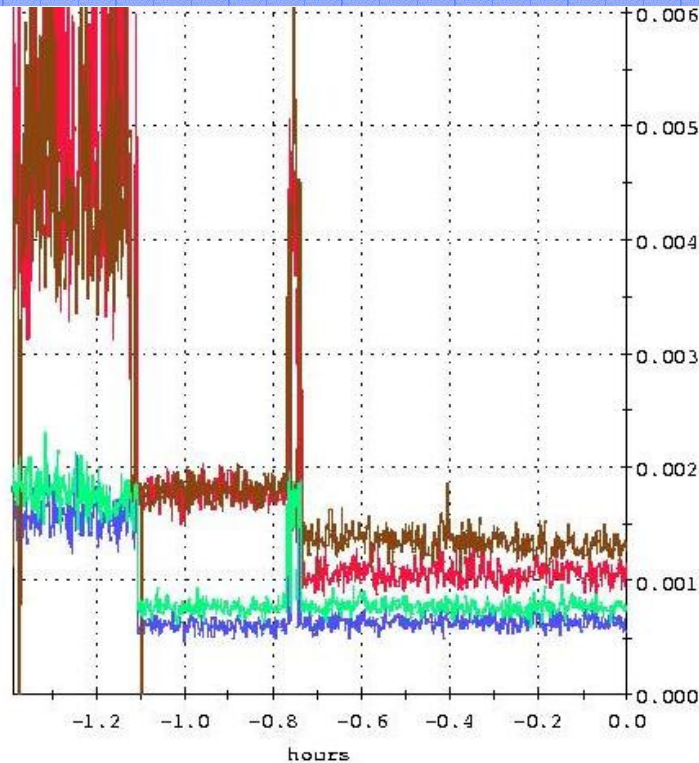
H plane results: correction better than with the local feedback at the feedback BPM locations



local feedback ON (left), global feedback ON (right)

rms value: integrated from .1 to 200Hz

Feedback efficiency



SR/D-FBPM/C24S/POSX (Y)
SR/D-FBPM/C24S/POSZ (Y)
SR/D-FBPM/C14S/POSX (Y)
SR/D-FBPM/C14S/POSZ (Y)

**rms stability in 2 sensitive ID
straight sections:**

Left : no feedback

Right: both feedback applied

red and brown:

horizontal rms position variation

blue and green:

horizontal rms position variation

Integrated from .1 to 200Hz

Next steps

- 1 **Addition of a selective damping of the 50Hz line in the DSP algorithm**
- 1 **Addition of more diagnostics functions (triggering of the BPMs recording on external events...)**

Conclusion

- 1 With a mix of feedforward action on the orbit perturbations, passive damping of the vibration of the magnets, and a fast orbit correction with a global feedback, we manage to still have a state of the art beam stability (even if our BPMs are now a bit outdated...).

System size for fast global correction:

All you need is:

- 1 4 KHz sampling for 200Hz BW
- 1 BPM and correctors number roughly equal to the integer of the tune value